## APPENDIX A

## % BEGINNING OF PSEUDO CODE

% compute scale factor A, and time constants a, b from physical system parameters

 $A = V_{max} * K_{t} / (R_{e} * R_{m} + K_{t} * K_{b}) * l * k;$ 

10 p1 = 
$$1/Jm/Ie * (-Ie * Rm - Re * Jm + sqrt(Ie^2 * Rm^2 - 2 * Re * Rm * Ie * Jm + Re^2 * Jm^2 - 4 * Kt * Kb * Ie * Jm)) / 2;$$

$$p2 = 1/Jm/Ie * (-Ie * Rm - Re * Jm - sqrt(Ie^2 * Rm^2 - 2 * Re * Rm * Ie * Jm + Re^2 * Jm^2 - 4 * Kt * Kb * Ie * Jm)) / 2;$$

15 
$$a = max(-p1,-p2)$$
  
 $b = min(-p1,-p2)$ 

% make initial guesses for step durations

% set maximum iteration count

° Nmax = 1000;

25

for j = 1:Nmax

% save old values of step time intervals

30 et3old = et3;

```
et2old = et2;
             etlold = etl;
             % iterate for switch times using fixed voltage level Vmax
5
             et3 = -log(1.0 / 2.0 - exp(-et1 * a) / 2 + exp(-et2 * a)) / a;
             et2 = 1/b * log(2.0) + 3 * et3 - 1/b * log(2 * exp(1/A * b * X) * exp(et3)
                     * b) - sqrt( 4.0) * sqrt(exp(1/A * b * X)) * exp(et3 * b) *
                     sqrt(exp(1/A * b * X) + exp(et3 * b)^2 - 2 * exp(et3 * b)));
             et1 = -(-2 * A * et2 + 2 * A * et3 - X) / A;
10
             if norm([et3old - et3 et2old - et2 et1old - et1], inf) <= eps * 2
                      break
              end
15
              if j==Nmax
                             error(['error - failure to converge after ', num2str(Nmax),'
                      iterations'])
              end
              end
20
              % round up pulse duration to nearest sample interval,
              % convert to intervals between steps to make sure that voltage
              % requirements will not increase (beyond Vmax).
              dt1=ceil((et1 - et2) / dt) * dt;
25
              dt2=ceil((et2 - et3) / dt) * dt;
              dt3=ceil((et3) / dt) * dt;
              et123 = [et1, et2, et3]
              % convert back to total step duration.
30
```

et1 = dt1 + dt2 + dt3; et2 = dt2 + dt3; et3 = dt3;

% In the following, the original constraints equations involving XF1, XF2, was and XF3 have been modified to include a variable voltage level applied

at

15

% each step (instead of the fixed maximum (+/-) Vmax).

10 % The original equations for XF1, XF2, and XF3 follow:

% 
$$XF_1(t_{end}) = V_0F_1(t_{tend} - t_0) - 2V_0F_1(t_{end} - t_1) + 2V_0F_1(t_{end} - t_2)$$

% 
$$XF_2(t_{end}) = V_0F_2(t_{tend} - t_0) - 2V_0F_2(t_{end} - t_1) + 2V_0F_1(t_{end} - t_2)$$

% 
$$XF_3(t_{end}) = V_0F_3(t_{tend} - t_0) - 2V_0F_2(t_{end} - t_1) + 2V_0F_1(t_{end} - t_2)$$

% And the modified equation including adjustable relative levels of voltage

% L1, L2 and L3 are:

% 
$$XF_1(t_{end}) = L_1V_0F_1(t_{tend} - t_0) - L_2V_0F_1(t_{end} - t_1) + L_3V_0F_1(t_{end} - t_2)$$

% 
$$XF_2(t_{end}) = L_1V_0F_2(t_{tend} - t_0) - L_2V_0F_2(t_{end} - t_1) + L_3V_0F_1(t_{end} - t_2)$$

20 
$$W_0 = V_0 F_3(t_{end}) = L_1 V_0 F_3(t_{tend} - t_0) - L_2 V_0 F_2(t_{end} - t_1) + L_3 V_0 F_1(t_{end} - t_2)$$

% And the corresponding constraint equations are:

$$% XF_1(t_{end}) = Finalpos$$

$$\% \qquad XF_2(t_{end}) = 0$$

25 % 
$$XF_3(t_{end}) = 0$$

% Where all of the times indicated have discrete values, e.g. corresponding to

% the controller update rate.

% It should be noted that after the digital switch times are fixed, the constraint

% equations derived from the equations above form a linear set of equations in

% the unknown relative voltage levels L1, L2 and L3 and any standard linear

% method can be used to solve for the relative voltage levels. In the equations

% for (L1, L2 and L3) that follow, the solution was obtained by algebraic % means (and are not particularly compact.)

% compute new relative voltage step levels

% L1, L2 and L3 are nominally assigned to "1", "-2" and "+2", respectively

15 
$$S1 = X * (exp(-et3 * b) * exp(-et2 * a) + exp(-et3 * a) + exp(-et2 * b) -exp(-et2 * b) * exp(-et3 * a) - exp(-et3 * b));$$

L1 = s1 \* s2;

5

20

25

```
\exp(-et2 * a) + \exp(-et3 * a) * et1 + \exp(-et2 * b) * et1 -
                           \exp(-\text{et2} * b) * \text{et1} * \exp(-\text{et3} * a) - \text{et3} * \exp(-\text{et1} * b) *
                           \exp(-\text{et2} * a) - \exp(-\text{et2} * a) * \text{et1} - \exp(-\text{et3} * b) * \text{et1} - \exp(-\text{et3} * a)
                 b) * et2 * \exp(-\text{et1} * a) + \text{et3} * \exp(-\text{et1} * b) + \text{et2} * \exp(-\text{et1} * a) +
                           \exp(-et3*b)*et2+et3*\exp(-et2*a))*X;
 5
                 (\exp(-et2 * b) * \exp(-et1 * a) - \exp(-et1 * a) - \exp(-et2 * b) -
                           \exp(-\text{et1 * b}) * \exp(-\text{et2 * a}) + \exp(-\text{et1 * b}) + \exp(-\text{et2 * a})) / A;
                  L3 = s1*s2;
       s1 = \exp(-et1 * a) - \exp(-et3 * a) + \exp(-et3 * b) - \exp(-et1 * b) -
10
                           \exp(-\text{et3} * b) * \exp(-\text{et1} * a) + \exp(-\text{et1} * b) * \exp(-\text{et3} * a);
       s2 = X / (et2 * exp(-et1 * b) * exp(-et3 * a) + exp(-et2 * b) * et3 *
                           exp(-et1 * a) - et2 * exp(-et3 * a) - et2 * exp(-et1 * b) - et3 *
                           \exp(-\text{et1} * a) - \exp(-\text{et2} * b) * \text{et3} + \exp(-\text{et3} * b) * \text{et1} * \exp(-\text{et2} * b)
                 a) + exp(-et3 * a) * et1 + exp(-et2 * b) * et1 - exp(-et2 * b) * et1 * exp(-
15
                 et3 * a) - et3 * exp(-et1 * b) * exp(-et2 * a) - exp(-et2 * a) * et1-exp(-et3 *
                 b) * et1 - \exp(-\text{et3} * \text{b}) * \text{et2} * \exp(-\text{et1} * \text{a}) + \text{et3} *
                           \exp(-\text{et1} * b) + \text{et2} * \exp(-\text{et1} * a) + \exp(-\text{et3} * b) * \text{et2} + \text{et3} *
                           \exp(-\text{et2} * a)) / A;
20
                 L2 = s1 * s2;
                 % convert accumulated voltage steps to sequential voltage level
                  V1 = Vmax * (L1);
25
                  V2 = Vmax * (L1 + L2);
                  V3 = Vmax * (L1 + L2 + L3);
                  % END OF PSEUDO CODE
```